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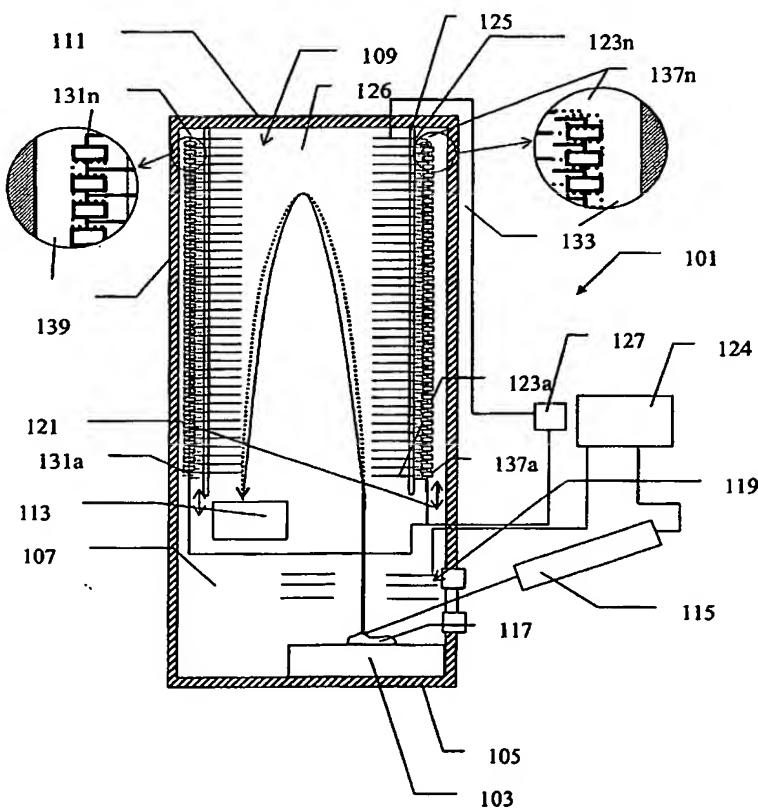
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## REFLECTRON

### Field of the Invention

The present invention relates to devices and methods of the type mentioned in the preambles of the independent claims for improving the resolution and sensitivity of mass spectrometers.

5

### Prior Art

Mass spectrometers can be used to determine the composition of samples. In some time-of-flight mass spectrometers (TOF MS) a sample is ionised in the first end of a mass spectrometer, the sample ions are accelerated by an electrical field towards the second end of

10 the mass spectrometer at a certain time, then retarded and turned around by a retarding electrical field in a reflectron at the second end of the mass spectrometer and the arrival time of the sample ions at a detector mounted outside the reflectron is recorded. The time between an ion being accelerated and it being detected at the detector is known as the time of flight for the ion and is dependent on, amongst others, the length of the flight path and the mass to

15 charge ratio of the ion. The resolution of a TOF MS is dependent on the spread of the flight times of ions of the same type. One of the main reasons for the spread of flight times is the difference in the lengths of the flight paths that the individual ions take. One of the variations in the length of the flight path is caused by the different radial positions of the ions when they are accelerated to the mass spectrometer detector surface. The sensitivity of a mass

20 spectrometer is a function of its signal to noise levels. Once source of random noise is chemical noise. This is noise caused by ions which disintegrate after they have started to be accelerated, forming fragment ions and neutral particles of random energy. These particles have random velocities and consequently random times-of-flight. These particles cause a continuous background signal in the spectrum of signals originating from un-fragmented ions.

25

If a mass spectrometer is provided with a linear reflectron configuration (i.e. the resistances between the series of parallel electrodes forming the reflectron are selected so that the electrical field inside the reflectron varies linearly up the reflectron) then the energy bandwidth is small. This means that ions or particles having kinetic energies which are 30 outside this bandwidth are not focused and consequently only in the order of 10% of the chemical noise is transferred to the detector at a peak position coinciding well with the parent ion.

If a mass spectrometer is provided with a quadratic reflectron configuration (i.e. the resistances of the series of parallel electrodes forming the reflectron are selected so that the electrical field inside the reflectron varies with a quadratic function up the reflectron) then the energy bandwidth is much larger than that of a mass spectrometer provided with a linear 5 reflectron and in the order of 80% of the chemical noise is transferred to the detector. This means that, if everything else is unchanged, if a quadratic reflectron in a mass spectrometer is replaced by a linear reflectron then this would theoretically lead to a maximum eightfold reduction in the single spectrum signal-to-noise ratio. Statistics show the signal-to-noise ratio (S/N) can be improved by increasing the number of measurements taken - the improvement in 10 the S/N ratio being proportional to the square root of the number of measurements taken. This means that in order to achieve an eightfold improvement in the S/N ratio to compensate for the reduction in the signal-to-noise ratio caused by changing from a linear reflectron to a quadratic reflectron by increasing the number of measurements, the number of measurements made would have been 64 times the original number of measurements. Thus using a quadratic 15 reflectron requires increased sample consumption and increased measurement times to achieve the same signal to noise ratio as a linear reflectron.

On the other hand, the use of a quadratic reflectron is preferred for post source decay (PSD) mass spectrometry, i.e. mass spectrometry in which molecules are excited after ionisation so 20 that they decay into fragments with a large energy spread during flight in the drift region of the mass spectrometer, as the high bandwidth of the quadratic reflectron allows the large energy spread to be shown on a single spectrum. A mass spectrometer equipped with a linear reflectron, with its low bandwidth, when used in PSD would require several (e.g. 10-15) spectra to be recorded at different reflectron voltages and the spectra combined to form a 25 single spectrum corresponding to the spectrum obtained from a mass spectrometer equipped with a quadratic reflectron.

However exchanging a linear reflectron for a quadratic reflectron causes a drop in bandwidth thus the designer of a mass spectrometer has hitherto been forced to choose between designing a 30 mass spectrometer with a high S/N ratio and narrow bandwidth or a relatively low S/N ratio and a relatively high bandwidth.

### Summary of the Invention

According to the present invention, at least some of the problems with the prior art are solved by means of a device having the features present in the characterising part of claim 1.

### 5 Brief Description of the Figures

Figure 1 shows schematically a cross-section through a prior art mass spectrometer provided with a reflectron; and,

Figure 2 shows schematically a cross-section through a mass spectrometer provided with an

10 reflectron in accordance with a second first embodiment of the present invention.

Table 1 shows an example of field resistances for forming a quadratic field inside a reflectron.

### Detailed Description of Embodiments Illustrating the Invention

15 Figure 1 shows a simplified schematic drawing (not to scale) of a prior art time-of-flight mass spectrometer (TOF MS) 1 provided with a reflectron in which some parts of the mass spectrometer which are not related to the present invention are omitted in order to facilitate illustration of the present invention. TOF MS 1 comprises a sample plate 3 mounted at a first end 5 of a elongated casing 7, a reflectron 9 mounted in the opposite end 11 of the casing and an ion detector 13 mounted between the sample plate 3 and the exit orifice of the reflectron 9.

20 Ionisation means e.g. a laser 15 are directed onto the sample plate 3 and can be operated to ionise a sample 17 positioned on the sample plate 3. Electrical field generating ion-accelerating means such as grid, plate or ring electrodes 19 are positioned between the sample plate 3 and the reflectron 9 and can be energised in order to accelerate ions 21 from

25 the sample plate 3 towards the reflectron 9. Reflectron 9 comprises a series of electrodes 23a-23n mounted in parallel, spaced apart on a number of mounting rods 25, with the planes of the electrodes 23 substantially perpendicular to the longitudinal axis of the casing 7. Mounting rods 25 are insulated so that they cannot conduct electricity between the electrodes 23. The centres of electrodes 23 are open in order to form a reflectron cavity 26 into which ions can

30 fly. Electrodes 23 are connectable to a reflectron high voltage power source 27 in order to produce an electrical field of opposite charge to the ions. This electrical field repels ions entering the central cavity, causing the ions to decelerate as they penetrate the cavity. When the high voltage power source 27 generates an electrical field over electrodes 23a-23n which

is of higher voltage than the voltage applied to accelerating means 19, then as the ions progress into the cavity 25 they will slow down, stop and then reverse direction. Ion detector 13 can be arranged to produce an output signal whenever ions of sufficient energy hit its detector surface 29. Laser 15, ion-accelerating means 19 and ion detector 13 are connectable to an automated remote control means such as a computer 24 which is programmable to operate the laser 15, to energise the ion-accelerating means 19 at an appropriate time to accelerate ions 21 towards the ion detector 13, and to record the ion arrival signals from the ion detector 13.

5

10 In order to control the path of the ions in the reflectron, the electrical field in the reflectron is designed to be of a specific shape, in this example a linear field. This linear field is achieved by calculating the resistance of each electrode 23a-23n needed to shape such a field and then arranging that every electrode 23a-23n is connectable to the reflectron high voltage power source via its own field resistance 31a-31n. Each of these field resistances 31a-31n is selected 15 to give its respective electrode 23a-23n the resistance necessary to form the desired field. For a linear field, each field resistance 31a-31n has the same value.

Figure 2 shows a simplified schematic drawing (not to scale) of a time-of-flight mass spectrometer (TOF MS) 101 provided with a reflectron in accordance with the present 20 invention in which some parts of the mass spectrometer which are not related to the present invention are omitted in order to facilitate illustration of the present invention. TOF MS 1 comprises a sample plate 103 mounted at a first end 105 of a elongated casing 107, a reflectron 109 mounted in the opposite end 111 of the casing and an ion detector 113 mounted between the sample plate 103 and the exit orifice of the reflectron 109. Ionisation means such 25 as a laser 115 are directed onto the sample plate 103 and can be operated to ionise a sample 117 positioned on the sample plate 103. Electrical field generating ion-accelerating means such as grids or plates 119 are positioned between the sample plate 103 and the reflectron 109 and can be energised in order to accelerate ions 121 from the sample plate 103 towards the reflectron 109. Reflectron 109 comprises a series of reflectron electrodes 123a-123n mounted 30 in parallel, spaced apart on a number of mounting rods 125, with the planes of the reflectron electrodes 123a-123n substantially perpendicular to the longitudinal axis of the casing 107. Mounting rods 125 are insulated so that they cannot conduct electricity between the reflectron electrodes 123. The centres of reflectron electrodes 123a-123n are open in order to form a

reflectron cavity 126 into which ions can fly. Reflectron electrodes 123 a-123n are connectable to a reflectron high voltage power source 127 in order to produce an electrical field of opposite charge to the ions. This electrical field repels ions entering the central cavity, causing the ions to decelerate as they penetrate the cavity. If the high voltage power source

5      127 generates an electrical field over reflectron electrodes 123a-123n which is of higher voltage than the voltage applied to accelerating means 119, then as the ions progress into the cavity 125 they will slow down, stop and then reverse direction. Ion detector 113 can be arranged to produce an output signal whenever ions of sufficient energy hit its detector surface 29. Laser 115, ion-accelerating means 119 and ion detector 113 are preferably all  
10     connected to an automated remote control means such as a computer 124 which is programmable to operate the laser 115, to energise the ion-accelerating means 119 at an appropriate time to accelerate ions 121 towards the ion detector 113, and to record the ion arrival signals from the ion detector 113.

15     In order to control the path of the ions in the reflectron, the electrical field in the reflectron must be of a specific shape, for example a linear field. An example of the path of an ion in a linear field is shown by a solid line in figure 2. This linear field is achieved by calculating the resistance of each reflectron electrode 123a-123n needed to shape such a field and then arranging that every reflectron electrode 123a-213n is connectable to the reflectron high  
20     voltage power source via its own first field resistance 131a-131n.. Each of the first field resistances 131a-131n is selected to give its respective reflectron electrode 123a-123n the resistance necessary to form the desired field. Each field resistance 131a-131n may be made up of one or more electrical resistors arranged to give the desired electrical resistance. For a linear field, each first field resistance 131a-131n has the same value e.g. R ohms. In this  
25     embodiment of the present invention, first field resistances 131a-131n are connected to a first movable rod 133. Rod 133 is connectable to the high voltage power source 127 and the first field resistances 131a-131n are arranged in series on rod 133. Rod 133 is movable from a first position (shown in solid lines in figure 2) in which the first field resistances 131a-131n are in contact with their respective reflectron electrodes 123a-123n to a second position (shown by  
30     dotted lines in figure 1) in which the first field resistances 131a-311n are not in contact with their respective reflectron electrodes 123a-123n.

In order to make it possible to change the bandwidth and signal-to-noise ratio of the mass spectrometer, a mass spectrometer in accordance with the present invention is provided with means for changing the shape of the electrical field in the reflectron, for example from a linear field to a quadratic field and vice versa. In the embodiment shown in fig. 2 this is achieved by

- 5 providing two different sets of field resistances which can be connected one set at a time to the reflectron electrodes (which can be plates or grids). For example, a quadratic field can be achieved by calculating the resistance of each reflectron electrode 123a-123n needed to shape such a field and then arranging that every reflectron electrode 123a-213n is connectable to the reflectron high voltage power source via its own second field resistance 137a-137n. Each of
- 10 the second field resistances 137a-137n is selected to give its respective reflectron electrode 123a-123n the resistance necessary to form the desired field. For a quadratic field, the second field resistances increase in value the further that they are from the entrance of the reflectron. Table 1 shows an example of the values of second field resistances 137a-137n which could be used to produce a quadratic field. An example of the path of an ion in a quadratic field is
- 15 shown by a dotted line in figure 2. In this embodiment of the present invention, second field resistances 137a-137n are connected to a second movable rod 139. Rod 139 is connectable to the high voltage power source 127 and the second field resistances 137a-137n are arranged in series on rod 133. Rod 139 is movable from a first position (shown in solid lines in figure 1) in which the second field resistances 137a-137n are not in contact with their respective
- 20 reflectron electrodes 123a-123n to a second position (shown by dotted lines in figure 1) in which the second field resistances 137a-137n are in contact with their respective reflectron electrodes 123a-123n.

In this embodiment of the present invention, the type of field inside the reflectron can be

- 25 selected by moving rods 133 and rod 139 so that the field resistances on one rod (e.g. rod 133) are in contact with the reflectron electrodes and form part of an electrical circuit with the reflectron high voltage power source while the resistances on the other rod (e.g. rod 139) are out of contact with the reflectron electrodes and therefore do not form a complete electrical circuit and consequently do not contribute to the electrical field in the reflectron.

30

In a second embodiment of the present invention, each of the first and second field resistances is electrically connectable to its respective reflectron electrode by a switch. These switches may be manually or remotely switchable so that the resistance of some or all of the reflectron

electrodes can be adjusted by selecting if the switches connect the first field resistances or the second field resistances to the reflectron electrodes.

In a third embodiment of the present invention, said first and second field resistances are  
5 arranged so that the resistance of some or all of the reflectron electrodes can be adjusted by arranging for them to be connectable firstly to a first set of field resistances arranged to produce a first type of field in the reflectron e.g. a linear field, and secondly to be connectable to said first set of field resistances and to be connectable simultaneously in parallel to a second set of field resistances whereby a second type of field, e.g. a quadratic field is able to  
10 be produced in the reflectron. For example, the first set of field resistances may comprise a set of substantially identical field resistances, each having a resistance e.g. R ohms, able to be individually connectable to reflectron electrodes. The second set of field resistances may have the resistances shown in Table 1 minus R ohms. In this way a quadratic field can be achieved by bringing the second set of field resistances into a parallel electrical connection with the  
15 first set of field resistances, and a linear field can be achieved by breaking the electrical circuit between the first and second sets of field resistances.

Other fields inside the reflectron may be achieved by adding third, fourth or more sets of field resistances to a reflectron. Some sets of field resistance may comprise fewer field resistances  
20 than there are reflectron electrodes, so that only a portion of the reflectron electrodes have their resistances changed and consequently only part of the electrical field inside the reflectron is changed when these sets of field resistances are connected and disconnected to the reflectron electrodes. For example, a first set of field resistances may be provided which contains at least one resistance per reflectron electrode, a second set of field resistances may  
25 be provided which contains at least one resistance per reflectron electrode, a third set of field resistances may be provided which contain at least one resistance for each of the reflectron electrodes in first portion, e.g. the half furthest away from the entrance to the reflectron, of the reflectron electrodes, and a fourth set of field resistances may be provided which contain at least one resistance for each of the reflectron electrodes in second portion, e.g. the half nearest  
30 to the entrance to the reflectron, of the reflectron electrodes. The first set of field resistances may be designed to form a linear field, the second set may be designed to form a quadratic field (either on their own or in combination with the first set), the third set may be designed to form a sharply rising linear field and the fourth set may be designed to form a less sharply

rising linear field. Using only the first set of field resistances would give a linear field throughout the reflectron. Using the first set and the third set would give a first linear field which rises at a first rate in the half of the reflectron nearest to the entrance to the reflectron, and a second linear field that rises at a second rate in the half of the reflectron furthest from the entrance to the reflectron. Using just the third and fourth set would give another first linear field in the half of the reflectron nearest to the entrance to the reflectron, and another second linear field that rises at another second rate in the half of the reflectron furthest from the entrance to the reflectron.

5 10 Other combinations of field resistors and sets of field resistors are also conceivable, including connecting individual field resistors and/or sets of field resistors and/or partial sets of field resistors in series and/or in parallel.

15 The above mentioned embodiments are intended to illustrate the present invention and are not intended to limit the scope of protection claimed by the following claims.

## Claims

1. Reflectron (109) for use in a mass spectrometer comprising a plurality of reflectron electrodes (123a-123n) connectable to one or more high voltage power supplies (127) characterised in that it is provided with means for changing the electrical potentials of at least some of said reflectron electrodes (123a-123n) in order to change the shape of the electrical field inside said reflectron (109).  
5
2. Reflectron in accordance with claim 1 characterised in that it is provided with at least two sets of field resistances (131a-131n, 137a-137n) which can be connected one set at a time, or in parallel, or in series, between the reflectron electrodes (123a-123n).  
10
3. Reflectron in accordance with claim 2 characterised in that one of said sets of field resistances comprises field resistances (131a-131n) arranged to produce a linear electrical field inside said reflectron (109).  
15
4. Reflectron in accordance with any of claims 2-3 characterised in that one of said sets of field resistances comprises field resistances (137a-137n) arranged to produce an essentially quadratic electrical field inside said reflectron (109).  
15
5. Reflectron in accordance with any of claims 2-4 characterised in that at least one of said sets of different resistances comprises fewer resistances than there are reflectron electrodes.  
20
6. Reflectron in accordance with any of the previous claims characterised in that at least one set of field resistances (131a-131n; 137a-137n) is mounted on a movable rod (133; 139), wherein said rod (133; 139) is movable between a first position where said set of field resistances (131a-131n; 137a-137n) are in electrical contact with said reflectron electrodes (123a-123n) and a second position where said set of field resistances (131a-131n; 137a-137n) is not in contact with said reflectron electrodes (123a-123n).  
25

<u>Field Resistor</u>	<u>Resistance</u>	<u>Field Resistor</u>	<u>Resistance</u>
Resistor 137a	910 ohms	Resistor 137ab	110000 ohms
Resistor 137b	3830 ohms	Resistor 137ac	113000 ohms
Resistor 137c	5490 ohms	Resistor 137ad	121000 ohms
Resistor 137d	7150 ohms	Resistor 137ae	127000 ohms
Resistor 137e	15000 ohms	Resistor 137af	130000 ohms
Resistor 137f	15800 ohms	Resistor 137ag	137000 ohms
Resistor 137g	18200 ohms	Resistor 137ah	147000 ohms
Resistor 137h	30100 ohms	Resistor 137ai	150000 ohms
Resistor 137i	31600 ohms	Resistor 137aj	158000 ohms
Resistor 137j	36500 ohms	Resistor 137ak	165000 ohms
Resistor 137l	38300 ohms	Resistor 137al	169000 ohms
Resistor 137l	44200 ohms	Resistor 137am	174000 ohms
Resistor 137m	51000 ohms	Resistor 137an	182000 ohms
Resistor 137n	51100 ohms	Resistor 137ao	187000 ohms
Resistor 137o	53600 ohms	Resistor 137ap	191000 ohms
Resistor 137p	54900 ohms	Resistor 137aq	196000 ohms
Resistor 137q	56200 ohms	Resistor 137ar	200000 ohms
Resistor 137r	61900 ohms	Resistor 137as	205000 ohms
Resistor 137s	66500 ohms	Resistor 137at	210000 ohms
Resistor 137t	698 00 ohms	Resistor 137au	221000 ohms
Resistor 137u	71500 ohms	Resistor 137av	232000 ohms
Resistor 137v	73200 ohms	Resistor 137aw	243000 ohms
Resistor 137w	82500 ohms	Resistor 137ax	249000 ohms
Resistor 137x	88700 ohms	Resistor 137ay	470000 ohms
Resistor 137y	90900 ohms	Resistor 137az	680000 ohms
Resistor 137z	93100 ohms	Resistor 137ba	910000 ohms
Resistor 137aa	100000 ohms	Resistor 137bb	1M ohms

Table 1

2/3

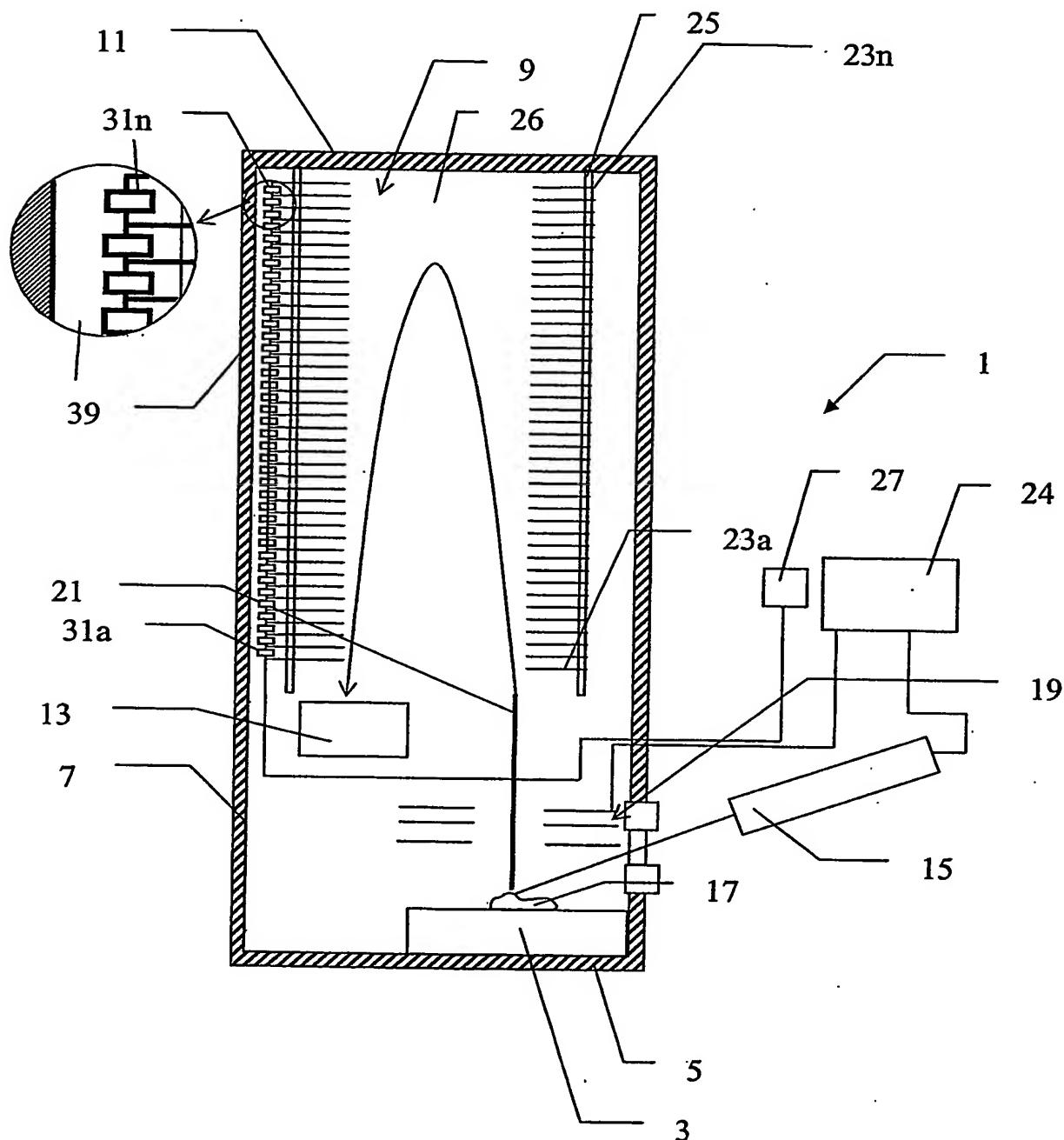


Fig. 1

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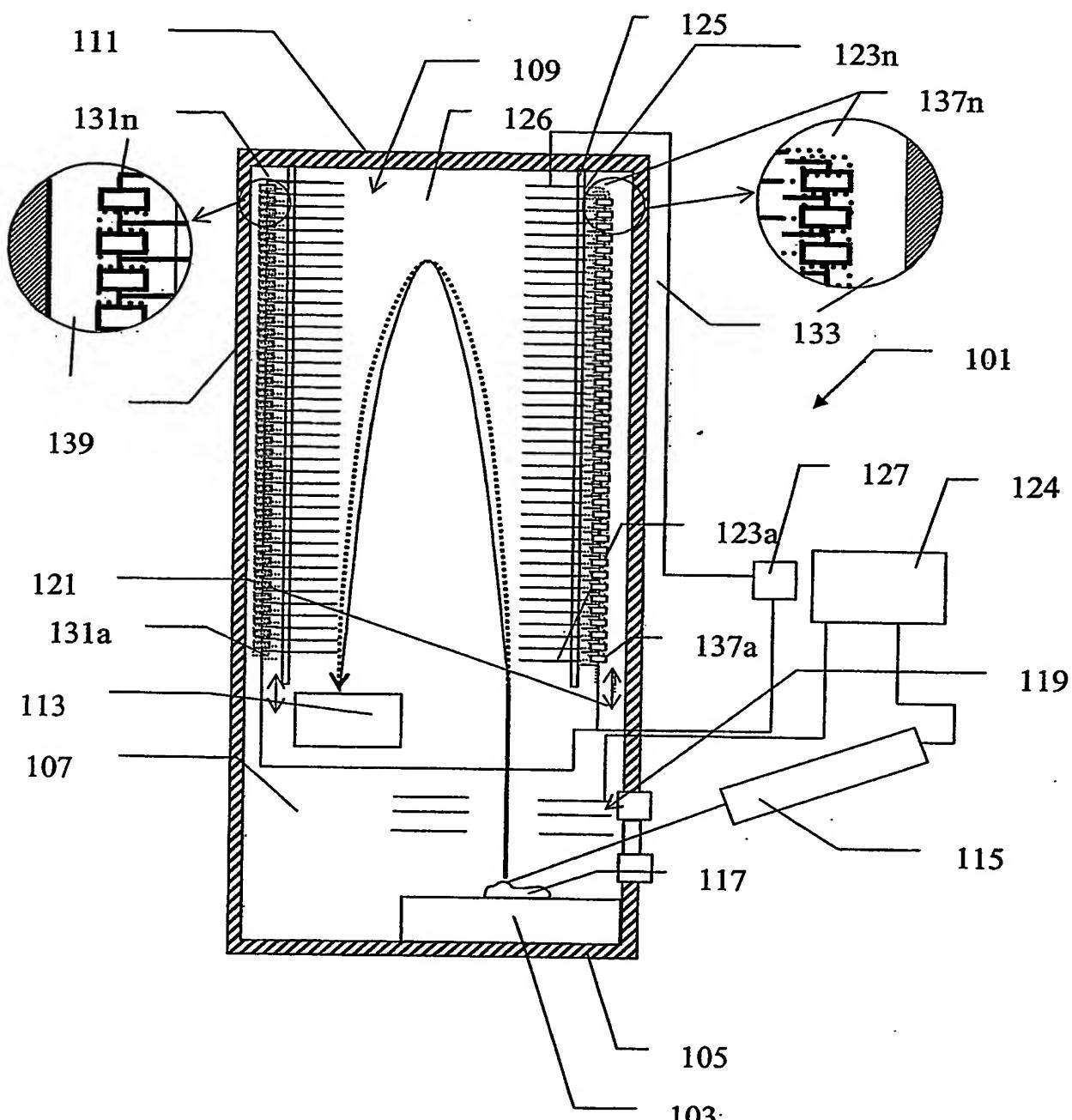


Fig. 2

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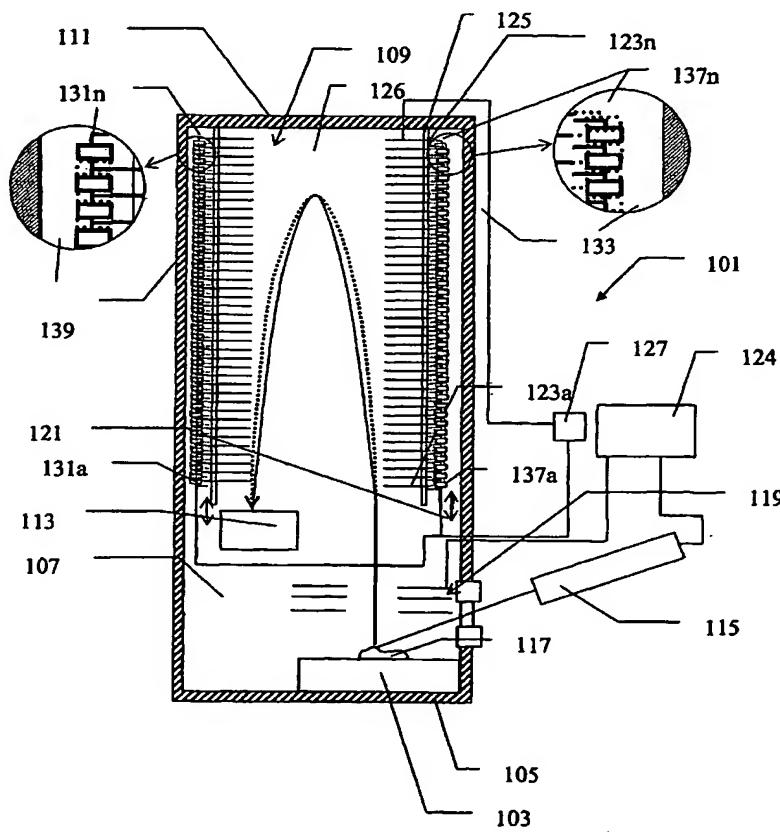
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[Continued on next page]

(54) Title: REFLECTRON



(57) Abstract: A reflectron (109) is provided with at least two sets of field resistances (131a-131n, 137a-137n) which may be connected together or separately to the reflectron electrodes (123a-123n) in order to be able to provide a plurality of different shaped electrical fields inside the reflectron (109).



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**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
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Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the International search (name of data base and, where practical, search terms used)

EPO-Internal

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 6 365 892 B1 (DOROSHENKO VLADIMIR M ET AL) 2 April 2002 (2002-04-02) column 3, line 60 -column 4, line 4 ---	1-6
A	US 6 013 913 A (HANSON CURTISS D) 11 January 2000 (2000-01-11) page 3, line 50 - line 67 column 6, line 7 - line 26 ---	1-6
A	WO 01 11660 A (GBC SCIENT EQUIP PTY LTD ;MAKAROV ALEXANDER A (GB)) 15 February 2001 (2001-02-15) page 4, line 8 - line 14 ---	1-6
A	US 5 814 813 A (CORNISH TIMOTHY J ET AL) 29 September 1998 (1998-09-29) the whole document ---	1-16
		-/-

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Patent family members are listed in annex.

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